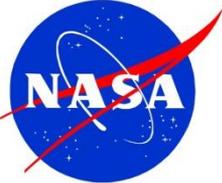


# **AePW-2: FUN3D Results**

**Pawel Chwalowski and Jennifer Heeg**  
**Aeroelasticity Branch, NASA Langley Research Center, Hampton, Virginia**

AIAA SciTech 2016, San Diego, CA



- ◆ Robert Biedron, Bil Kleb, Beth Lee-Rausch, and Eric Nielsen from the Aerosciences Branch at NASA Langley
- ◆ Steve Massey from Aeroelasticity Branch
- ◆ Dave Schuster from NESC
- ◆ NAS, NASA Advanced Supercomputing Center



# AePW-2 Cases

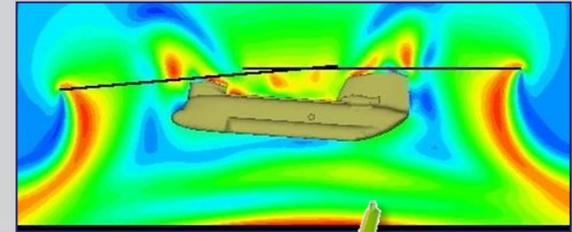


	Case 1	Case 2	Optional Case 3		
			A	B	C
Mach	0.7	0.74	0.85	0.85	0.85
Angle of attack	3	0	5	5	5
Dynamic Data Type	Forced Oscillation	Flutter	Unforced Unsteady	Forced Oscillation	Flutter
Notes:	<ul style="list-style-type: none"> <li>Attached flow solution</li> <li>Oscillating Turn Table (OTT) exp. data</li> </ul>	<ul style="list-style-type: none"> <li>Unknown flow state</li> <li>Pitch and Plunge Apparatus (PAPA) exp. data</li> </ul>	<ul style="list-style-type: none"> <li>Separated flow effects</li> <li>Oscillating Turn Table (OTT) experimental data</li> </ul>	<ul style="list-style-type: none"> <li>Separated flow effects</li> <li>Oscillating Turn Table (OTT) experimental data</li> </ul>	<ul style="list-style-type: none"> <li>Separated flow effects on aeroelastic solution</li> <li>No experimental data for comparison</li> </ul>

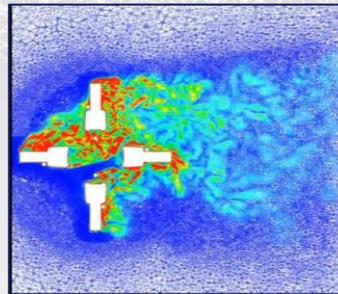
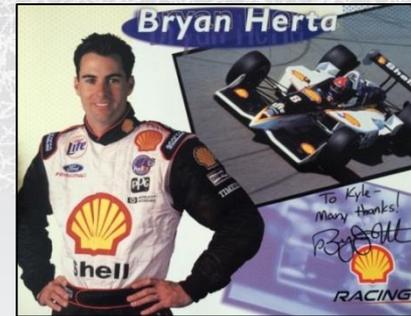
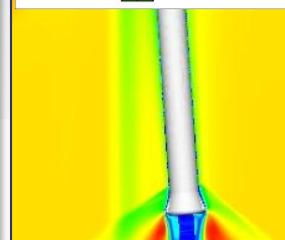
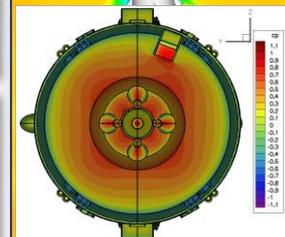
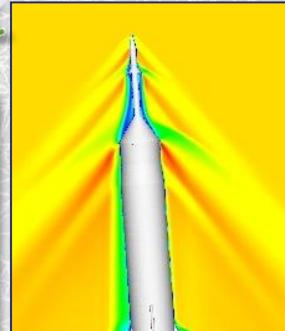
# FUN3D Core Capabilities

<http://fun3d.larc.nasa.gov/>

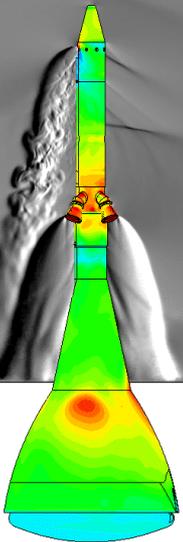
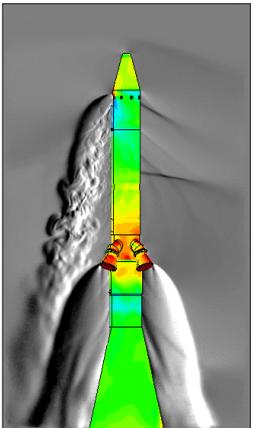
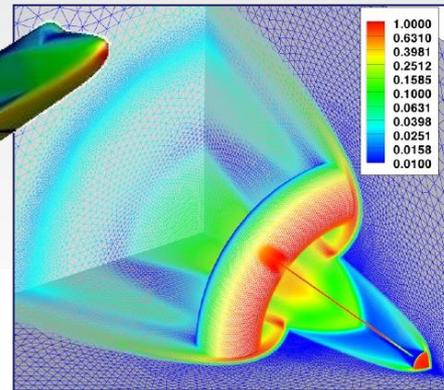
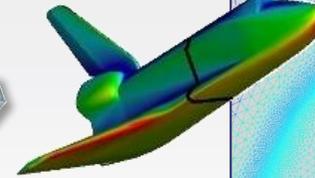
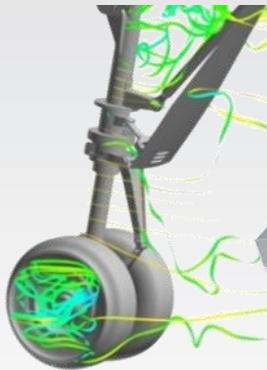
- Established as a research code in late 1980s; now supports numerous internal and external efforts across the speed range
- Solves 2D/3D steady and unsteady Euler and RANS equations on node-based mixed element grids for compressible and incompressible flows
- General dynamic mesh capability: any combination of rigid / overset / morphing grids, including 6-DOF effects
- Aeroelastic modeling using mode shapes, full FEM, etc.
- Constrained / multipoint adjoint-based design and mesh adaptation
- Distributed development team using agile/extreme software practices including 24/7 regression, performance testing
- Capabilities fully integrated, online documentation, training videos, tutorials



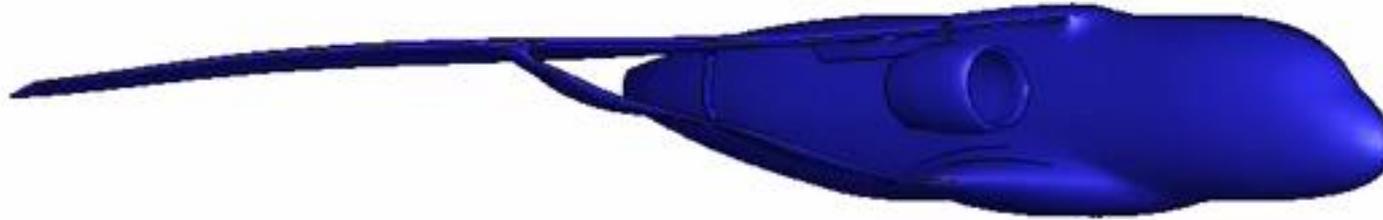
US Army



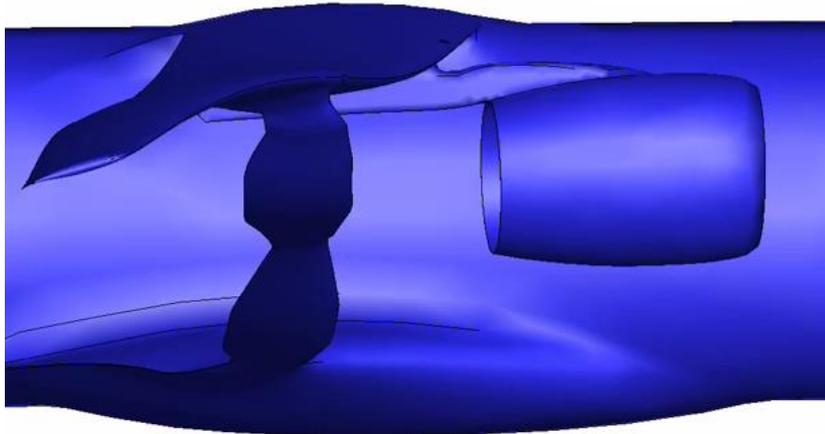
Georgia Tech



# Some Recent NASA Applications

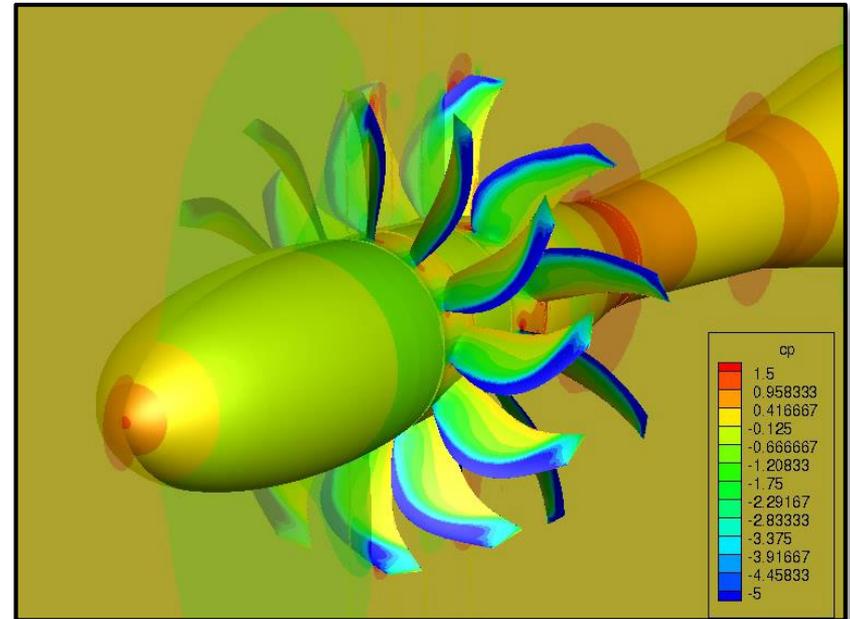


Courtesy  
Bob Bartels



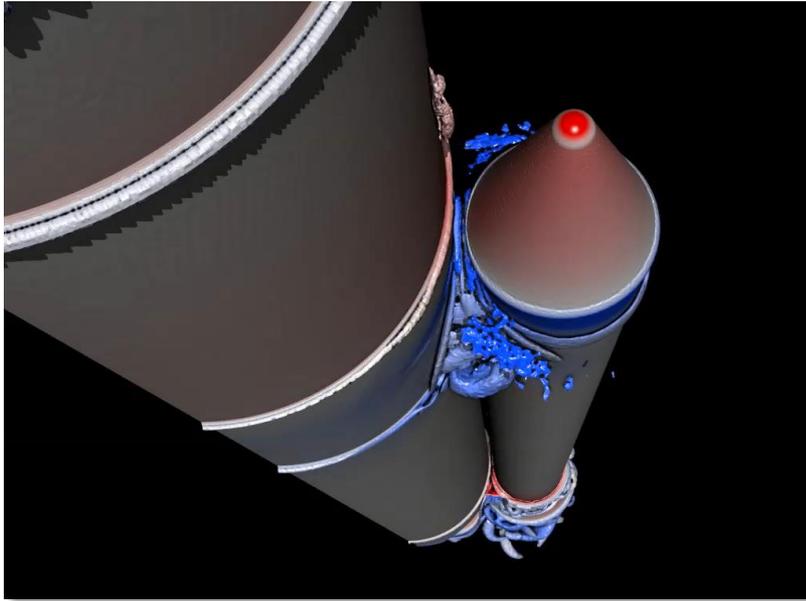
***Aeroelastic Analysis of  
the Boeing SUGAR  
Truss-Braced Wing  
Concept***

***Open-Rotor Concepts***



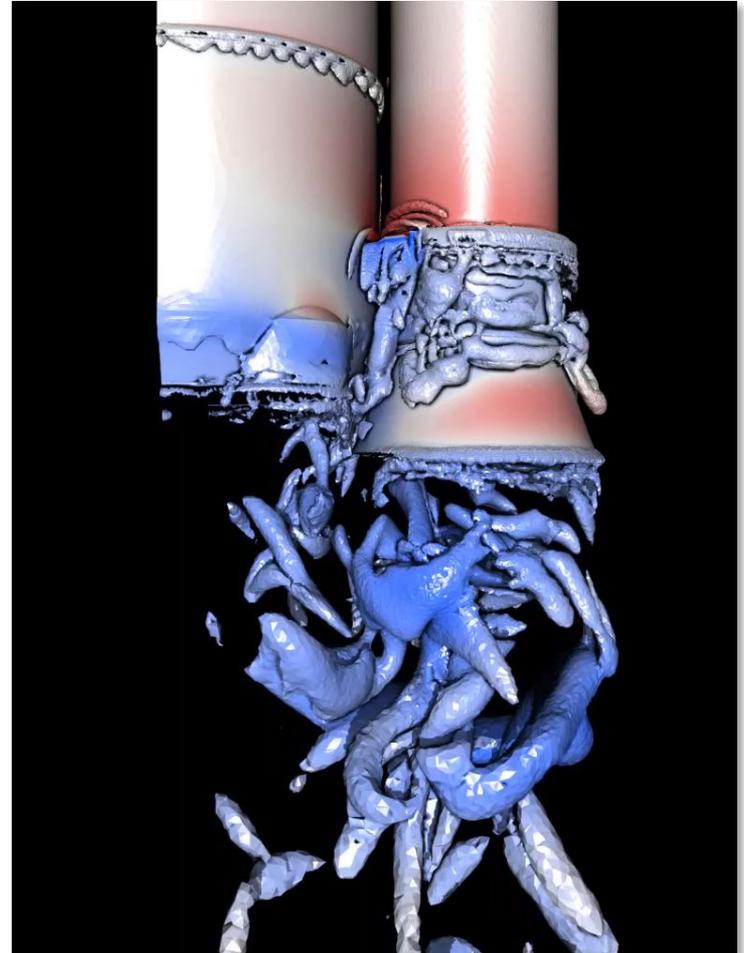
Courtesy Bill Jones

# Some Recent NASA Applications

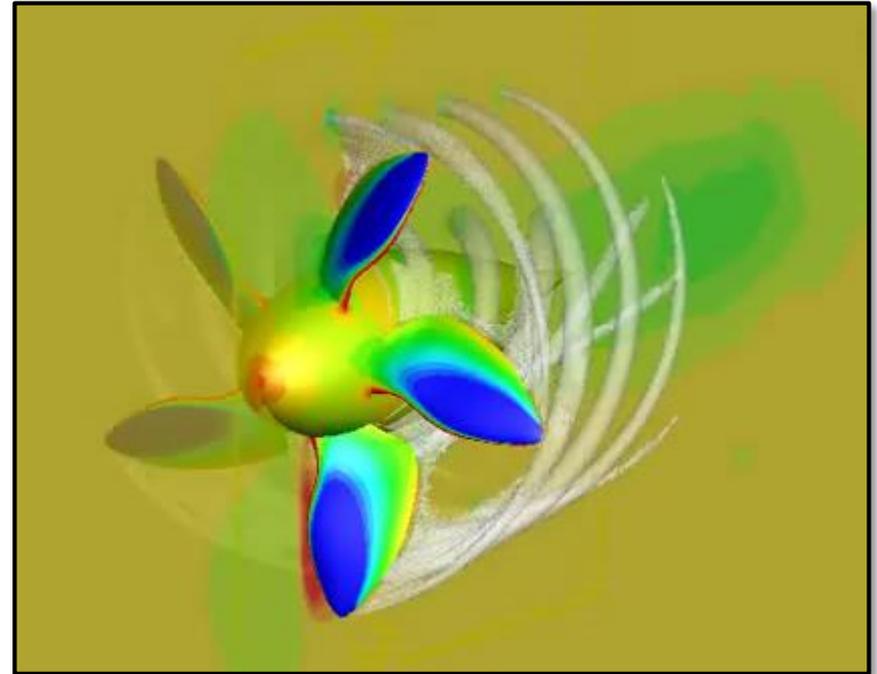


## ***Transonic Buffet Characterization for Space Launch System***

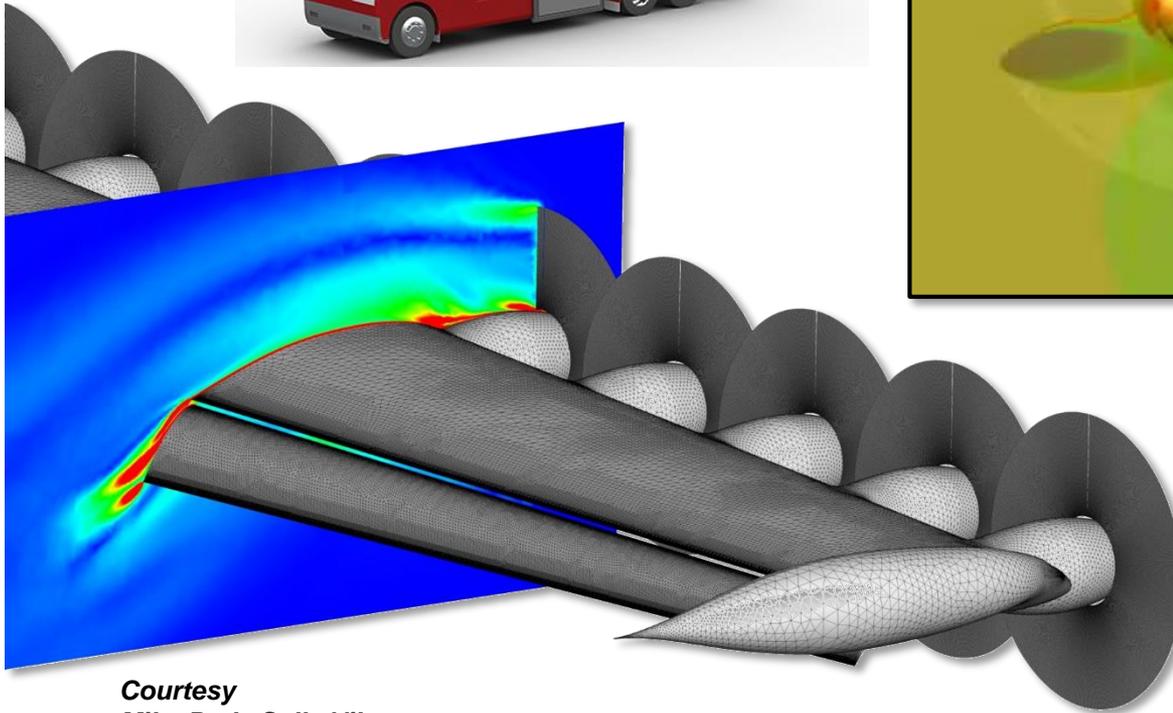
*Courtesy  
Greg Brauckmann,  
Steve Alter, Bil Kleb*



# Some Recent NASA Applications



*Courtesy Bill Jones*



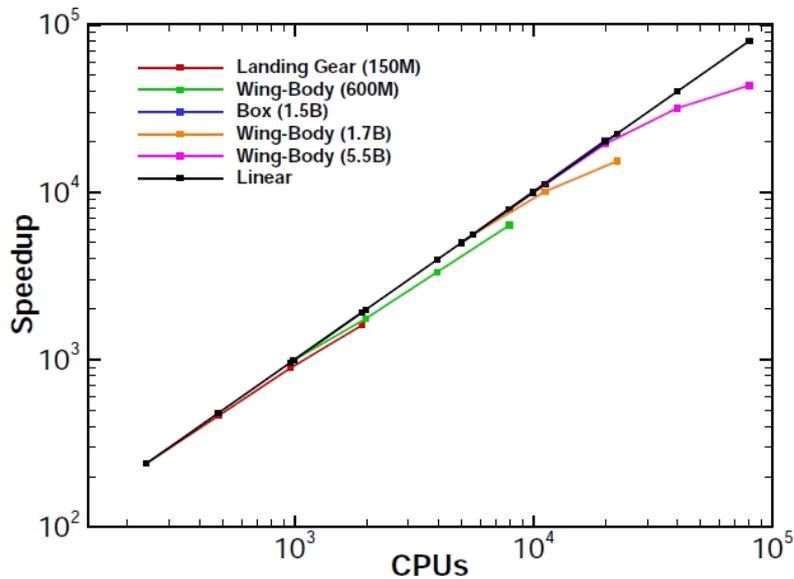
*Courtesy  
Mike Park, Sally Viken,  
Karen Deere, Mark Moore*

***Distributed Electric  
Propulsion***



# FUN3D and High-Performance Computing

***FUN3D is used on a broad range of HPC installations around the country***



***Scaled to 80,000 cores***





- ◆ Built upon elasticity PDE-based mesh deformation
- ◆ Built in modal structural solver, same as in CAP-TSD, CFL3D, Overflow
  - Typically uses mode shapes from NASTRAN normal modes analysis
- ◆ Coupling to external FEM/CSD codes
  - Read surface displacements obtained from FEM
  - Write aerodynamic loads ( $C_p$ ,  $C_{fx}$ ,  $C_{fy}$ ,  $C_{fz}$ ) for FEM
  - Requires CFD/CSD transfer middleware
  - Special case: rotorcraft comprehensive CSD codes, CAMRAD, DYMORE

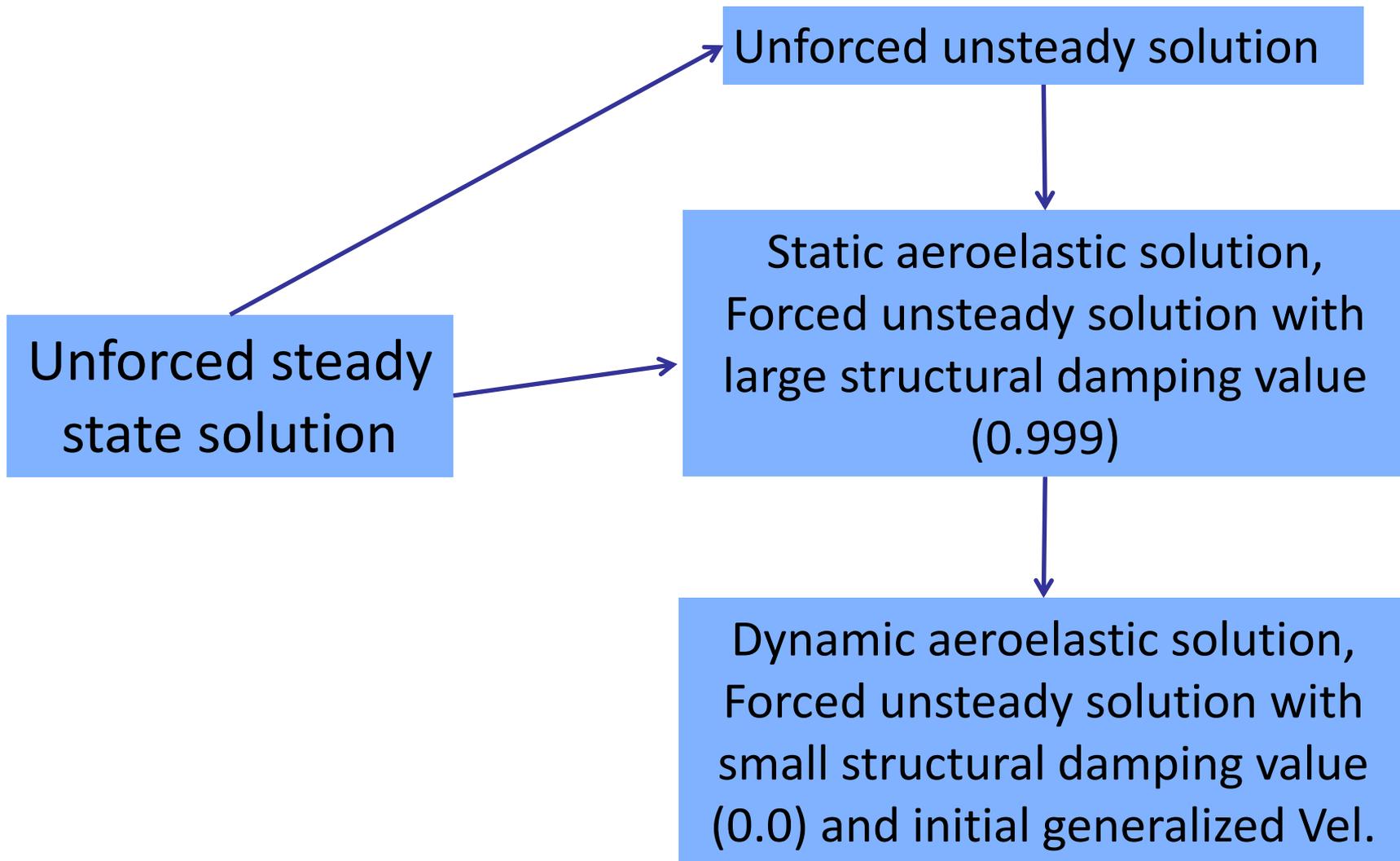
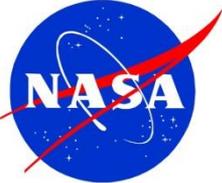


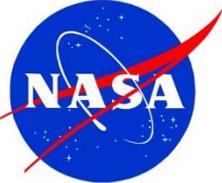
- ◆ Model the mesh as a linear elastic solid governed by

$$\nabla \cdot [\mu(\nabla u + \nabla u^T) + \lambda(\nabla \cdot u)I] = f = 0$$

$$l = \frac{Eu}{(1+\nu)(1-2\nu)} \quad m = \frac{E}{2(1+\nu)}$$

- ◆ Choose Poisson's ratio and Young's modulus to close system
  - $\nu = \text{const}, E = E(1/V) \text{ or } E(1/d)$
  - Smaller cells or cells closer to surface are stiffer
- ◆ Solve linear PDE
  - Large fraction (typ. 30% or more) of cost of flow-solver step
  - Eventually will employ multigrid to speed up solution
- ◆ Geometric Conservation Law (ALE formulation) accounted for
  - Essential for free stream preservation on deforming meshes
  - Appears as a source term in flow equation residuals

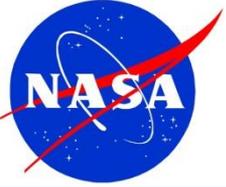




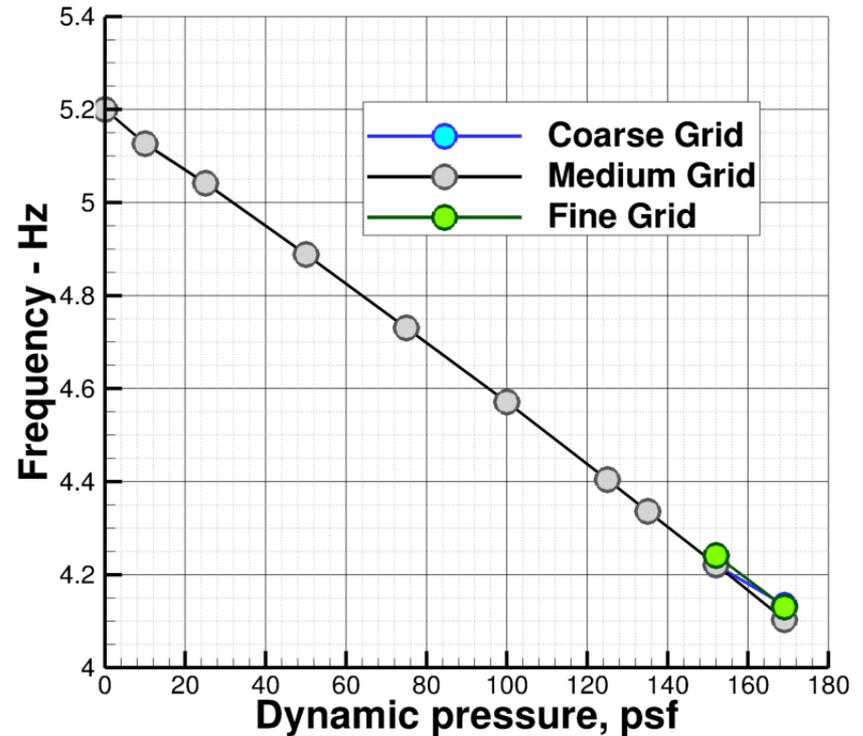
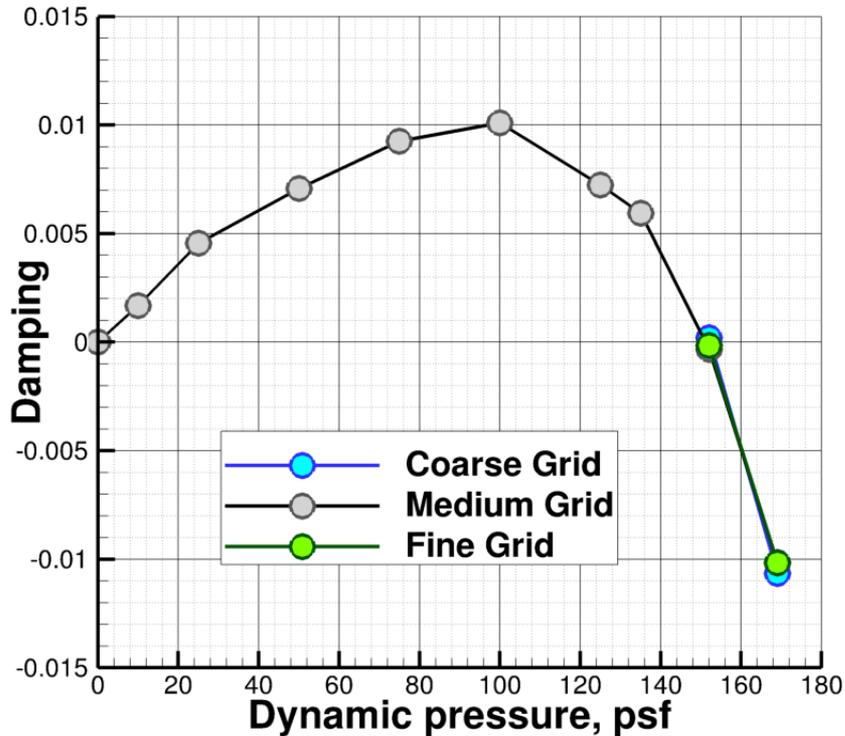
# AePW-2 Case 2, Mach 0.74, AoA = 0°



	Case 1	Case 2	Optional Case 3		
			A	B	C
Mach	0.7	0.74	0.85	0.85	0.85
Angle of attack	3	0	5	5	5
Dynamic Data Type	Forced Oscillation	Flutter	Unforced Unsteady	Forced Oscillation	Flutter
Notes:	<ul style="list-style-type: none"><li>Attached flow solution</li><li>Oscillating Turn Table (OTT) exp. data</li></ul>	<ul style="list-style-type: none"><li>Unknown flow state</li><li>Pitch and Plunge Apparatus (PAPA) exp. data</li></ul>	<ul style="list-style-type: none"><li>Separated flow effects</li><li>Oscillating Turn Table (OTT) experimental data</li></ul>	<ul style="list-style-type: none"><li>Separated flow effects</li><li>Oscillating Turn Table (OTT) experimental data</li></ul>	<ul style="list-style-type: none"><li>Separated flow effects on aeroelastic solution</li><li>No experimental data for comparison</li></ul>



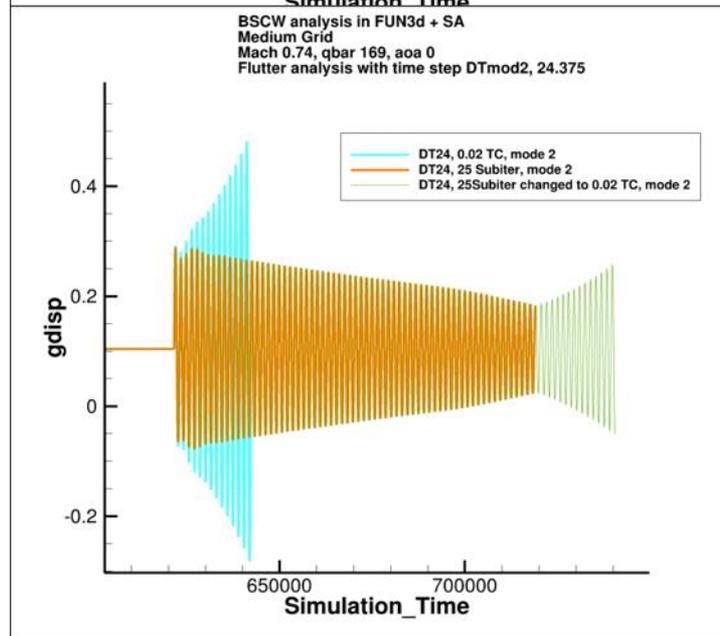
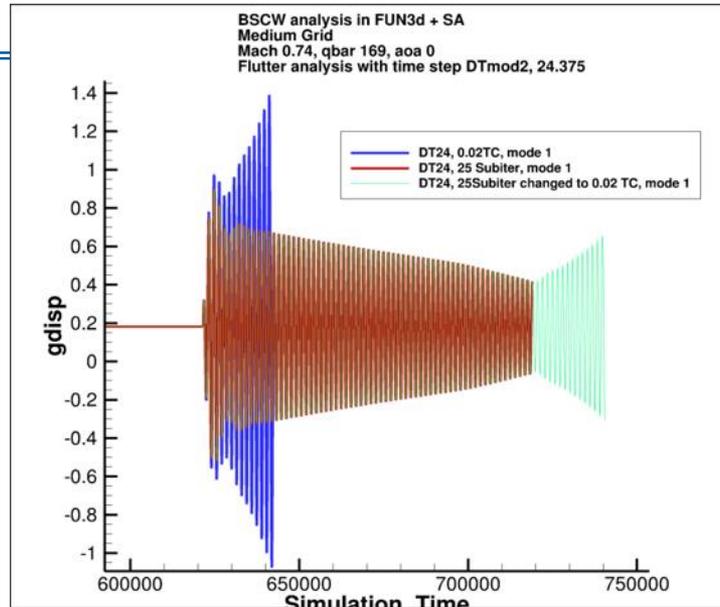
# AePW-2 Case 2, Mach 0.74, AoA = 0°



Predicted flutter onset:  $q = 152$  psf and  $f = 4.23$  Hz



# AePW-2 Case 2, Mach 0.74, AoA = 0°

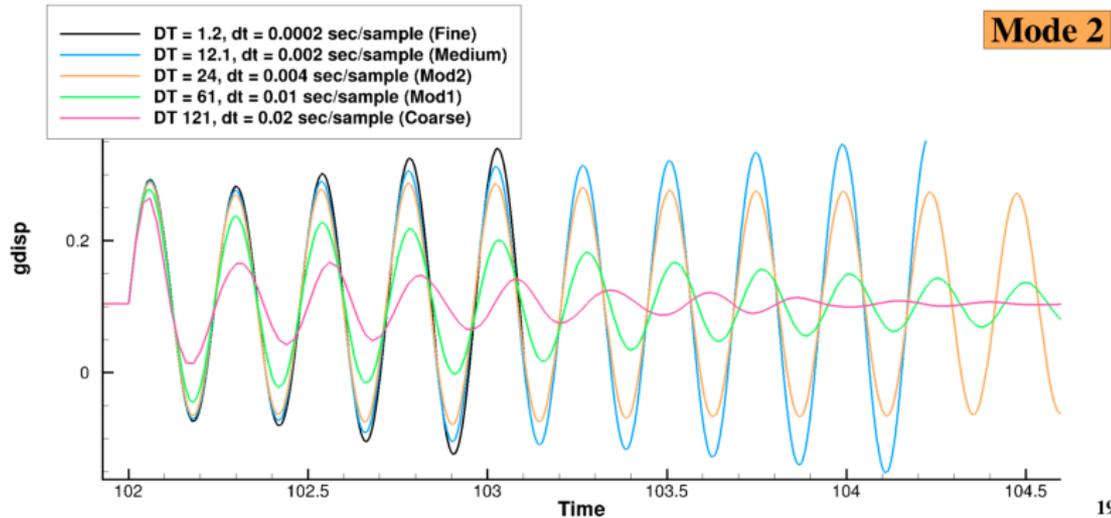
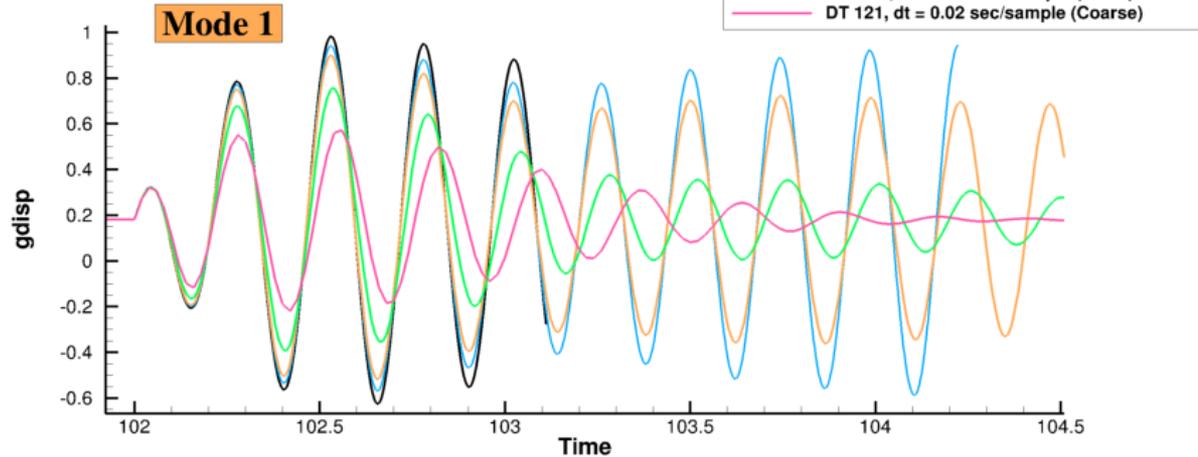




# AePW-2 Case 2, Mach 0.74, AoA = 0°

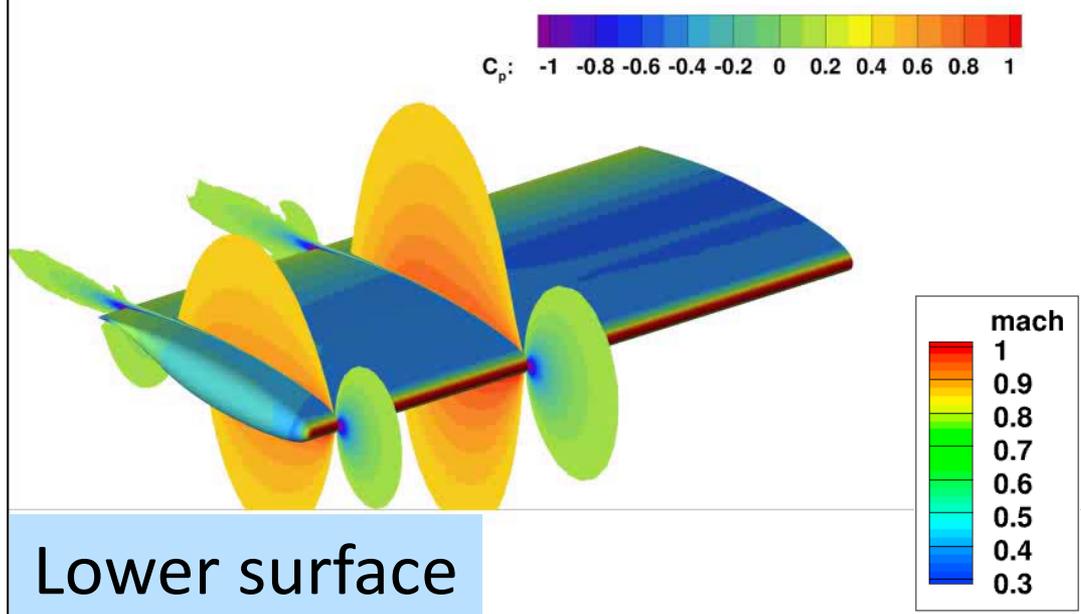


**BSCW FUN3D URANS + SA Dynamic Aeroelastic Analysis**  
Medium Grid  
Mach 0.74, Mean angle of attack 0 degs,  
Dynamic pressure 168.8 psf

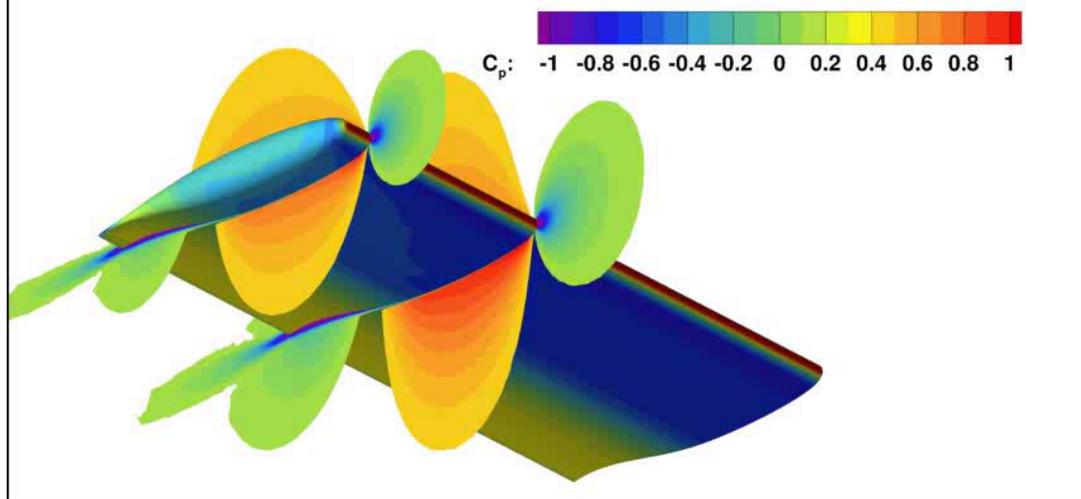




### Upper surface



### Lower surface





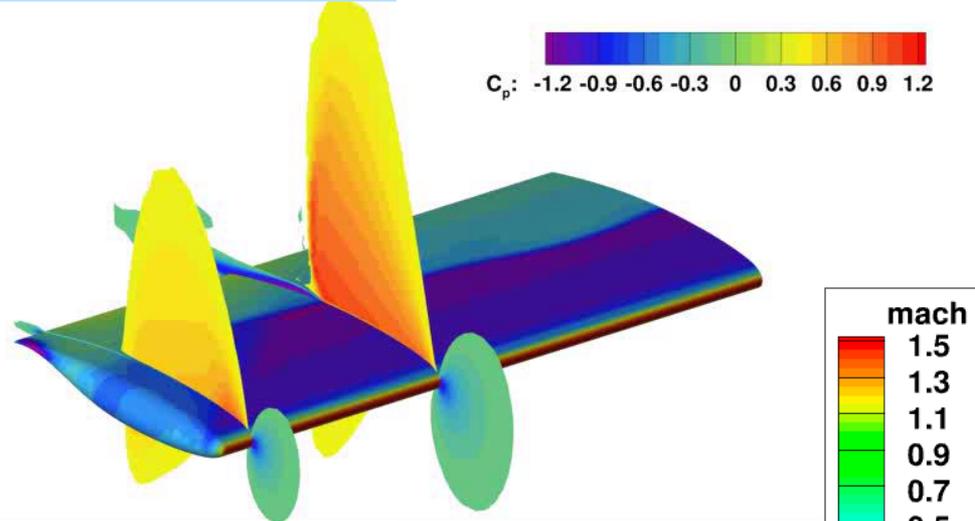
# AePW-2 Case 3B, Mach 0.85, AoA = 5°



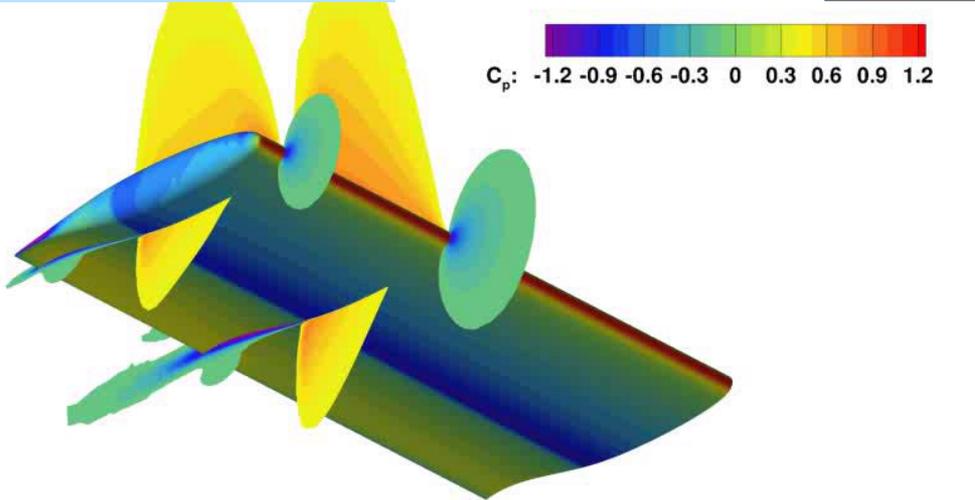
	Case 1	Case 2		Optional Case 3	
			A	B	C
Mach	0.7	0.74	0.85	0.85	0.85
Angle of attack	3	0	5	5	5
Dynamic Data Type	Forced Oscillation	Flutter	Unforced Unsteady	Forced Oscillation	Flutter
Notes:	<ul style="list-style-type: none"><li>Attached flow solution</li><li>Oscillating Turn Table (OTT) exp. data</li></ul>	<ul style="list-style-type: none"><li>Unknown flow state</li><li>Pitch and Plunge Apparatus (PAPA) exp. data</li></ul>	<ul style="list-style-type: none"><li>Separated flow effects</li><li>Oscillating Turn Table (OTT) experimental data</li></ul>	<ul style="list-style-type: none"><li>Separated flow effects</li><li>Oscillating Turn Table (OTT) experimental data</li></ul>	<ul style="list-style-type: none"><li>Separated flow effects on aeroelastic solution</li><li>No experimental data for comparison</li></ul>



### Upper surface



### Lower surface





# AePW-2 Case 3C, Mach 0.85, AoA = 5°



	Case 1	Case 2		Optional Case 3	
			A	B	C
Mach	0.7	0.74	0.85	0.85	0.85
Angle of attack	3	0	5	5	5
Dynamic Data Type	Forced Oscillation	Flutter	Unforced Unsteady	Forced Oscillation	Flutter
Notes:	<ul style="list-style-type: none"><li>Attached flow solution</li><li>Oscillating Turn Table (OTT) exp. data</li></ul>	<ul style="list-style-type: none"><li>Unknown flow state</li><li>Pitch and Plunge Apparatus (PAPA) exp. data</li></ul>	<ul style="list-style-type: none"><li>Separated flow effects</li><li>Oscillating Turn Table (OTT) experimental data</li></ul>	<ul style="list-style-type: none"><li>Separated flow effects</li><li>Oscillating Turn Table (OTT) experimental data</li></ul>	<ul style="list-style-type: none"><li>Separated flow effects on aeroelastic solution</li><li>No experimental data for comparison</li></ul>

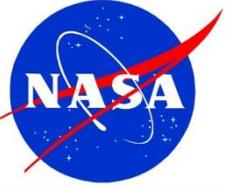


# AePW-2 Case 3C, Mach 0.85, AoA = 5°

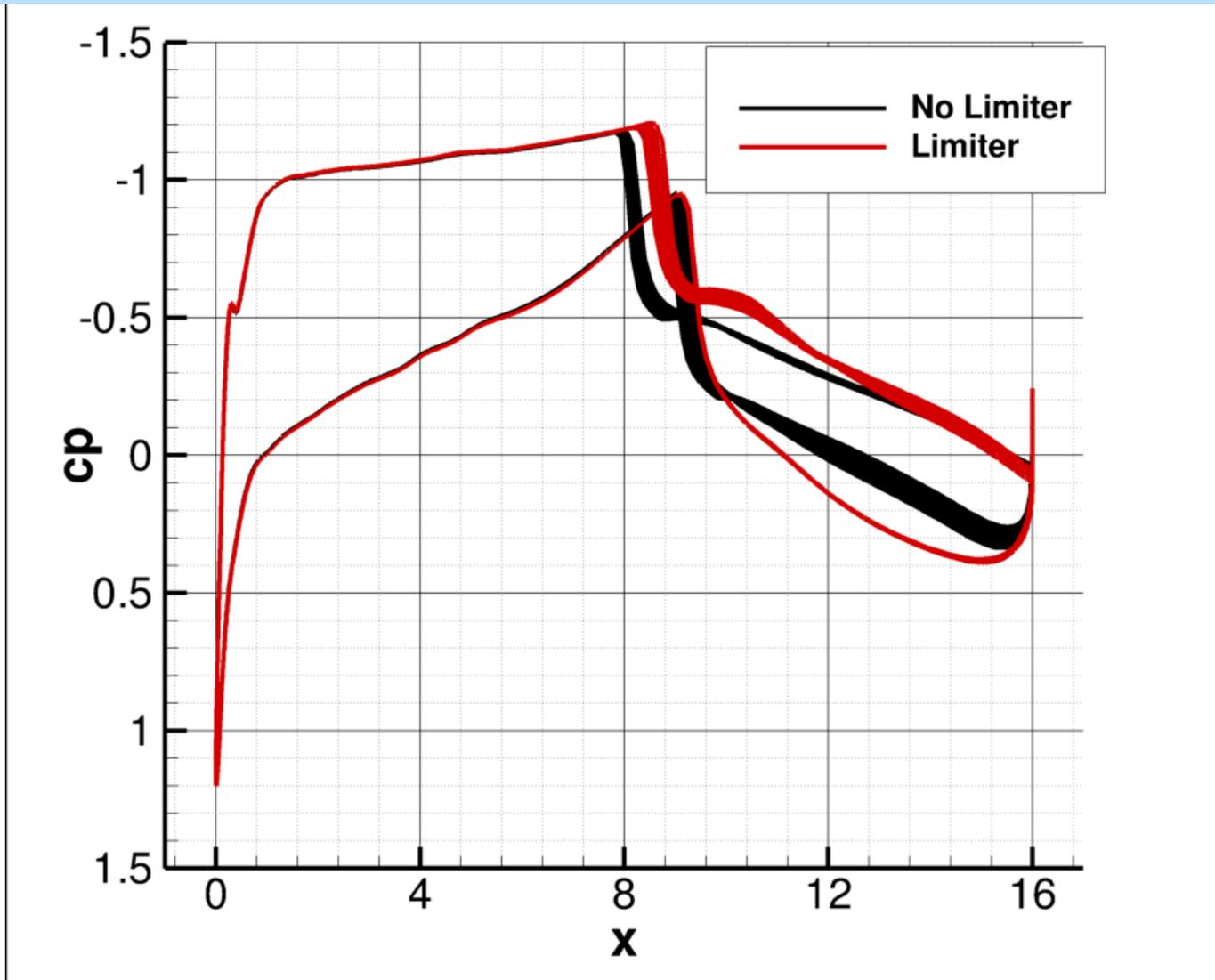


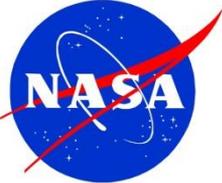
Mesh / Turb. Model	Flutter dynamic pressure, psf		Flutter frequency, Hz	
	No Limiter	Limiter	No Limiter	Limiter
Coarse / SA	455	665	4.85	4.65
Medium / SA	477	503	5.2	5.1
Fine / SA	390	482	5.0	4.8
Fine / DDES	565	x	5.1	x

Note: Venkatakrishnan Limiter

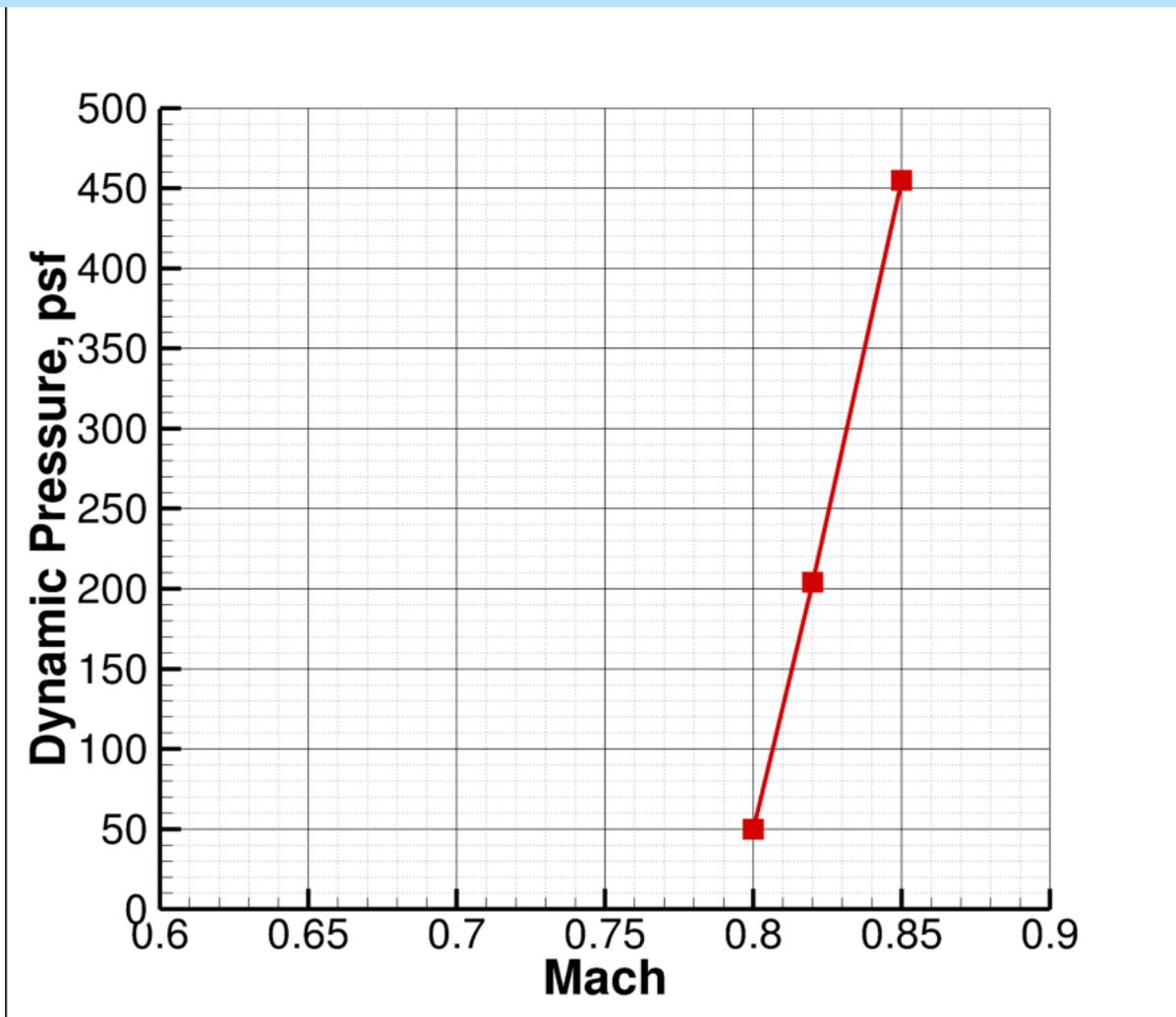


Static aeroelastic solution at q's near flutter onset: fine grids





Flutter Onset at AoA = 5°, Coarse Grid, No Limiter



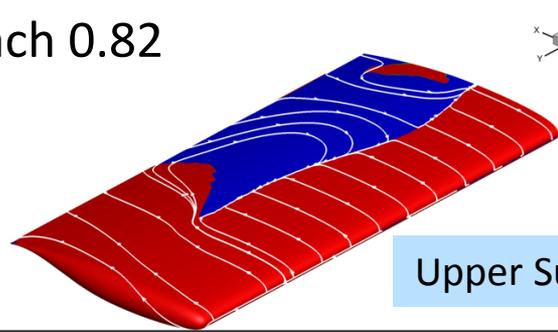


# AePW-2 Case 3C, Mach 0.85, AoA = 5°

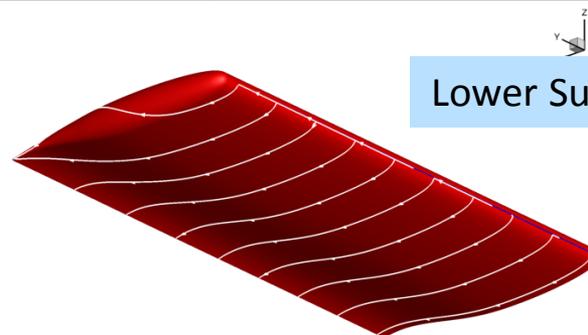


Static aeroelastic solutions:  
Skin friction and streamlines  
at dynamic pressure  
near flutter onset

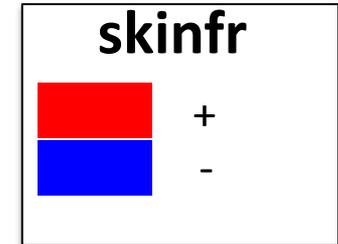
Mach 0.82



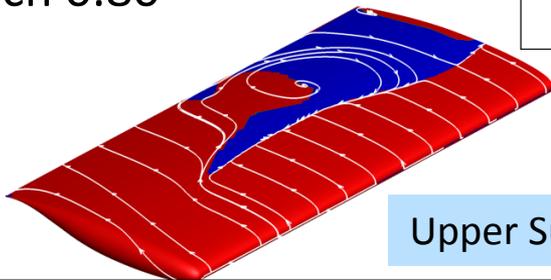
Upper Surface



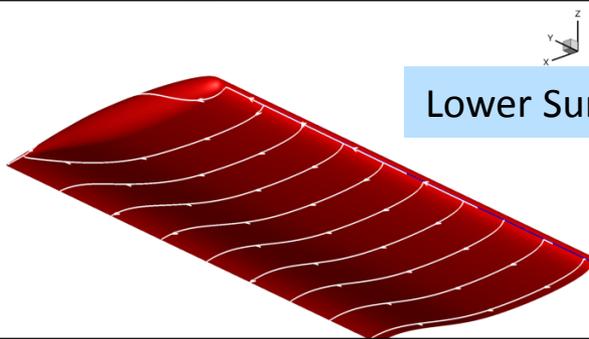
Lower Surface



Mach 0.80

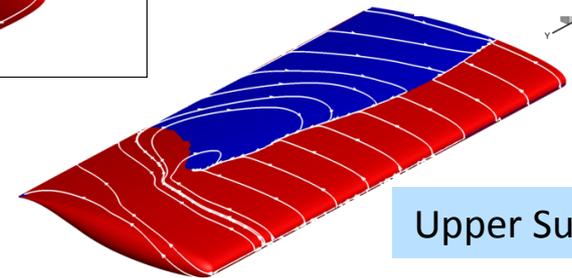


Upper Surface

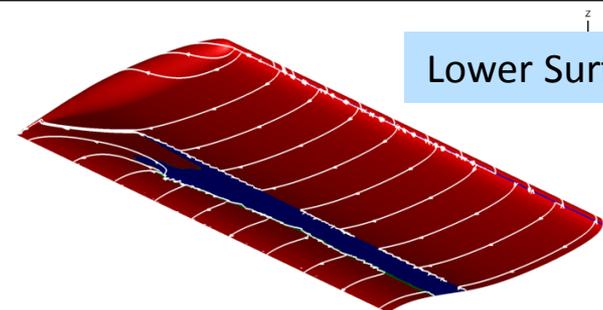


Lower Surface

Mach 0.85



Upper Surface



Lower Surface



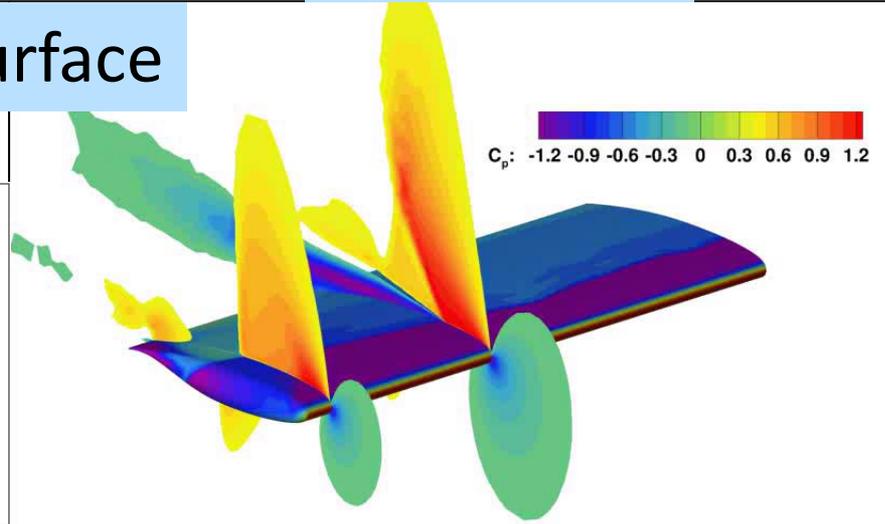
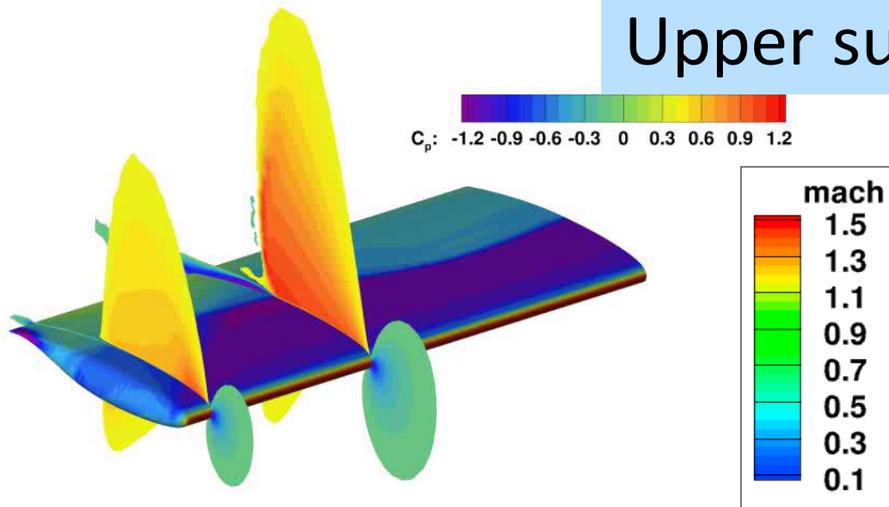
# AePW-2 Case 3C, Mach 0.85, AoA = 5°



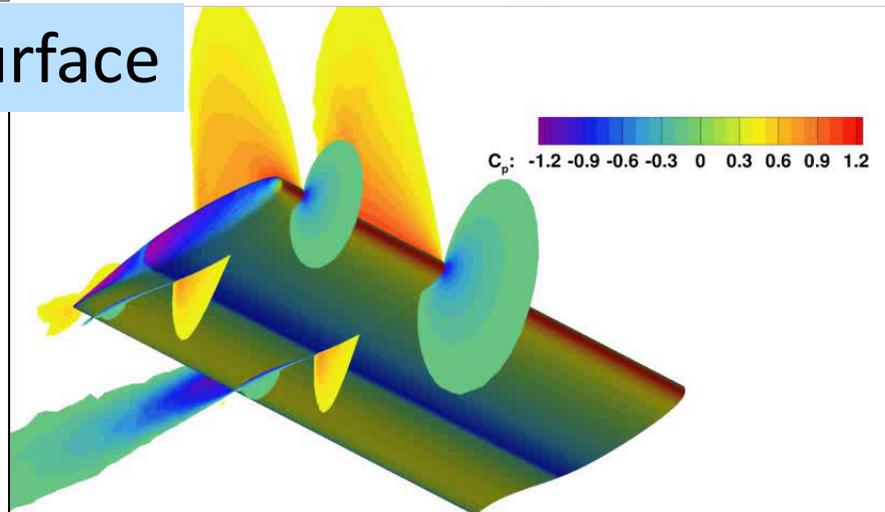
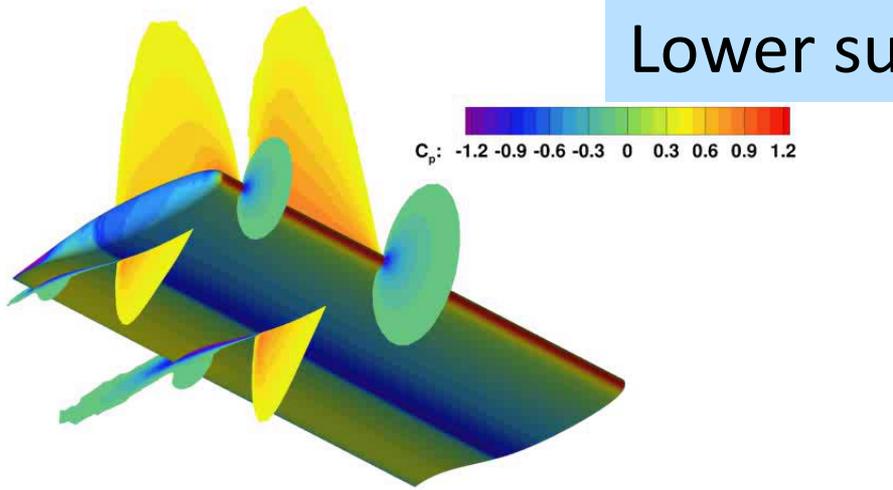
Q = 204 psf

Q = 816 psf

Upper surface



Lower surface

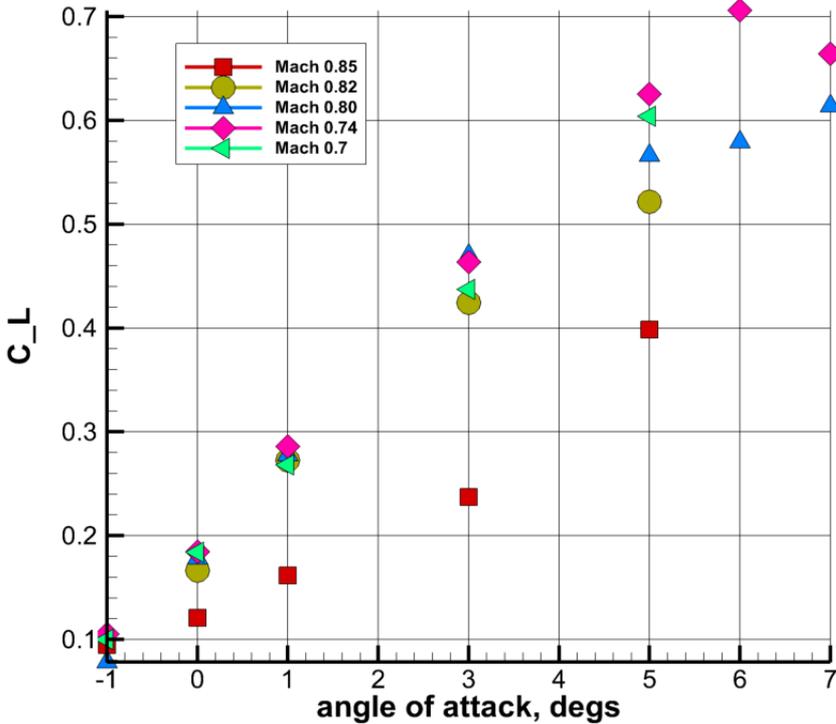




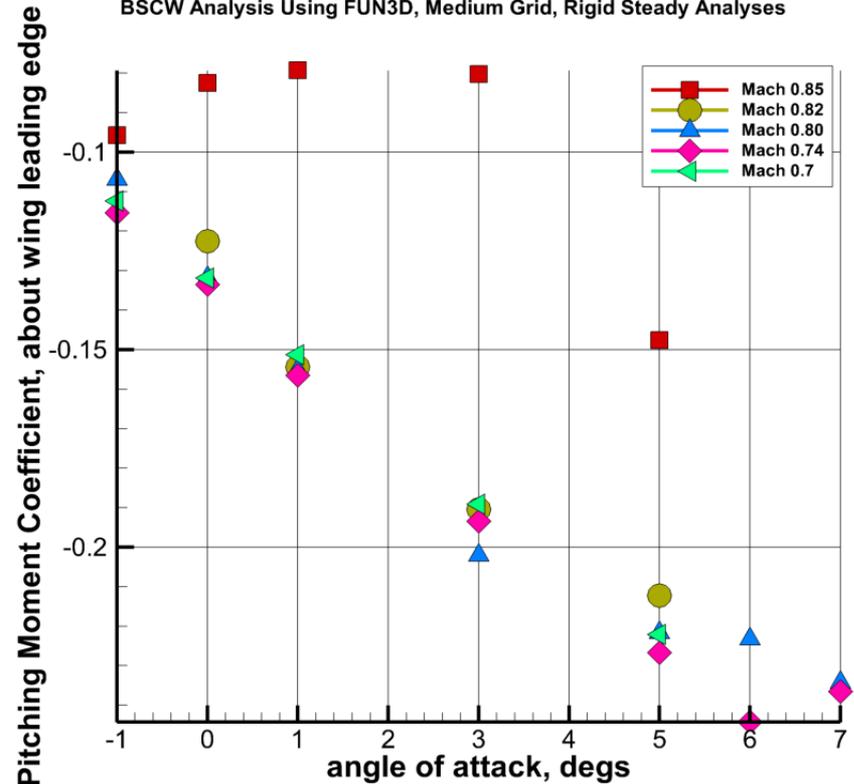
- ◆ It takes too long and significant computational resources are required to obtain flutter boundary prediction on a simple configuration like BSCW.
- ◆ There is need for tools like Reduced Order Methods to obtain flutter boundary prediction quickly.
- ◆ Spatial and temporal convergence analysis are necessary.
- ◆ 2D airfoil section analysis vs. 3D analysis.

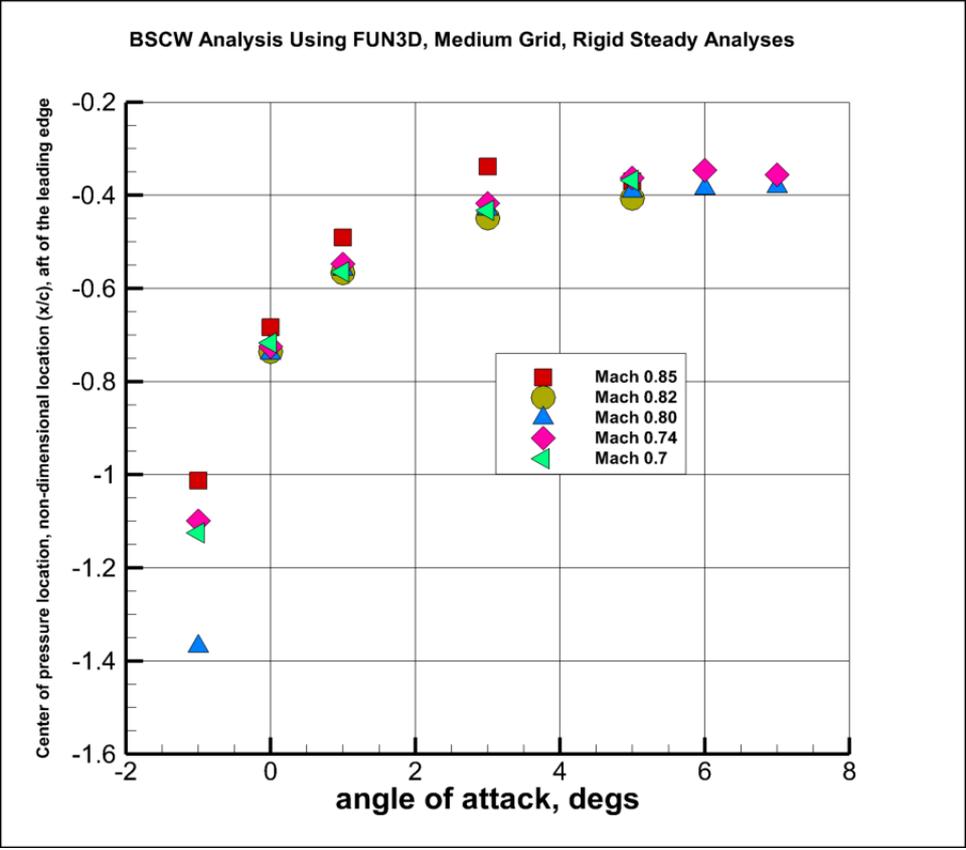


BSCW Analysis Using FUN3D, Medium Grid, Rigid Steady Analyses



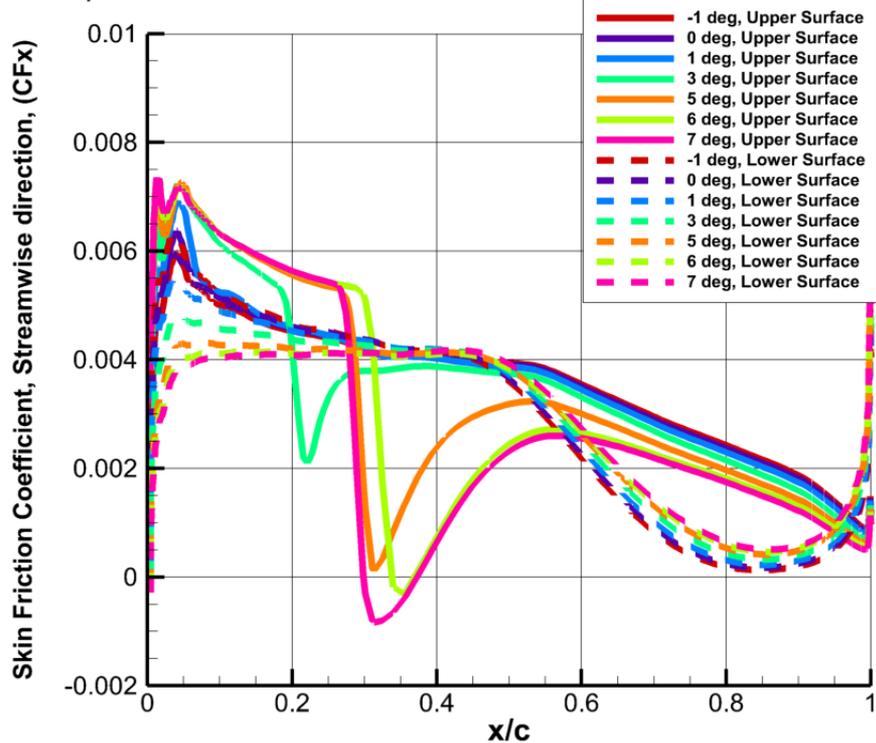
BSCW Analysis Using FUN3D, Medium Grid, Rigid Steady Analyses



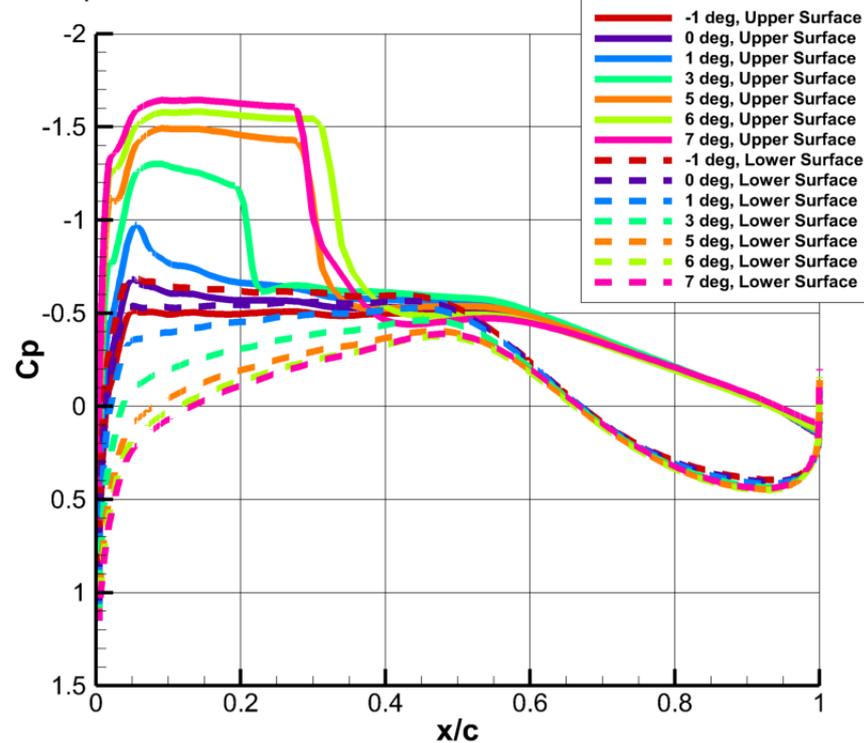


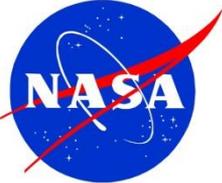


FUN3D Analysis, Medium Grid, Mach 0.74, Steady Rigid Analysis  
60% span station

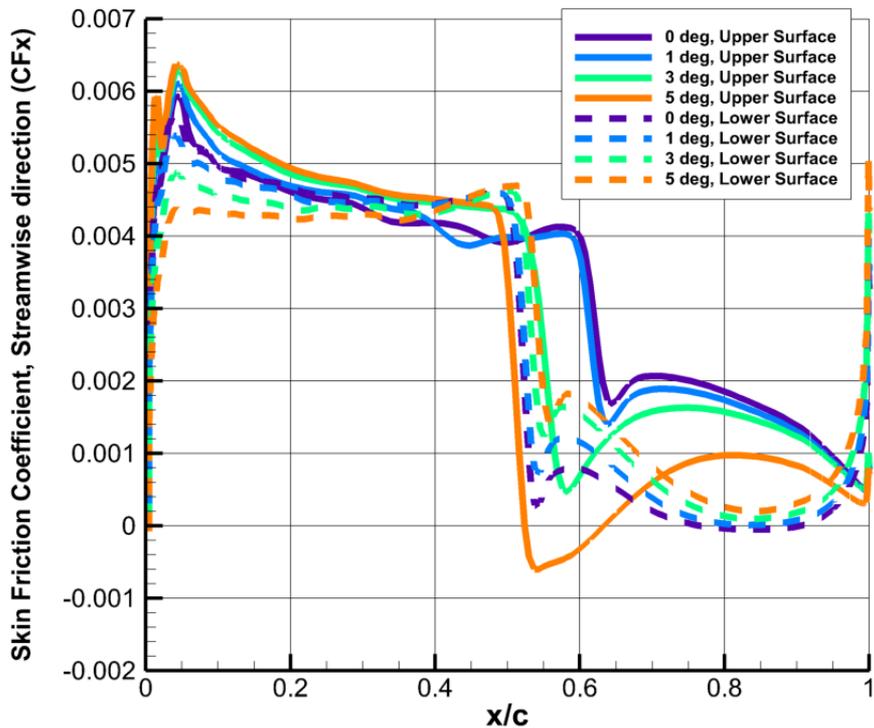


FUN3D Analysis, Medium Grid, Mach 0.74, Steady Rigid Analysis  
60% span station

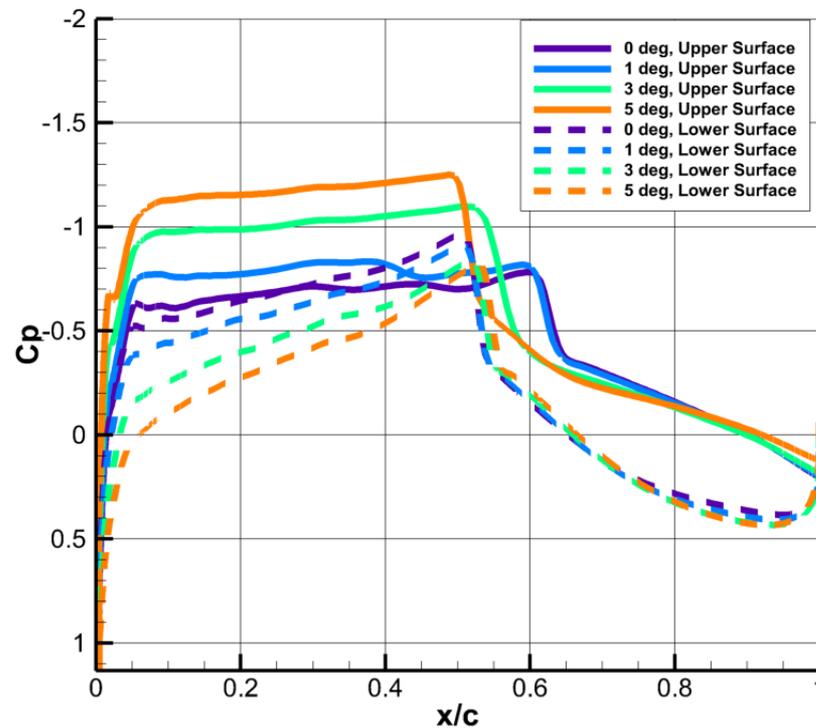




FUN3D Analysis, Medium Grid, Mach 0.82, Steady Rigid Analysis  
60% span station

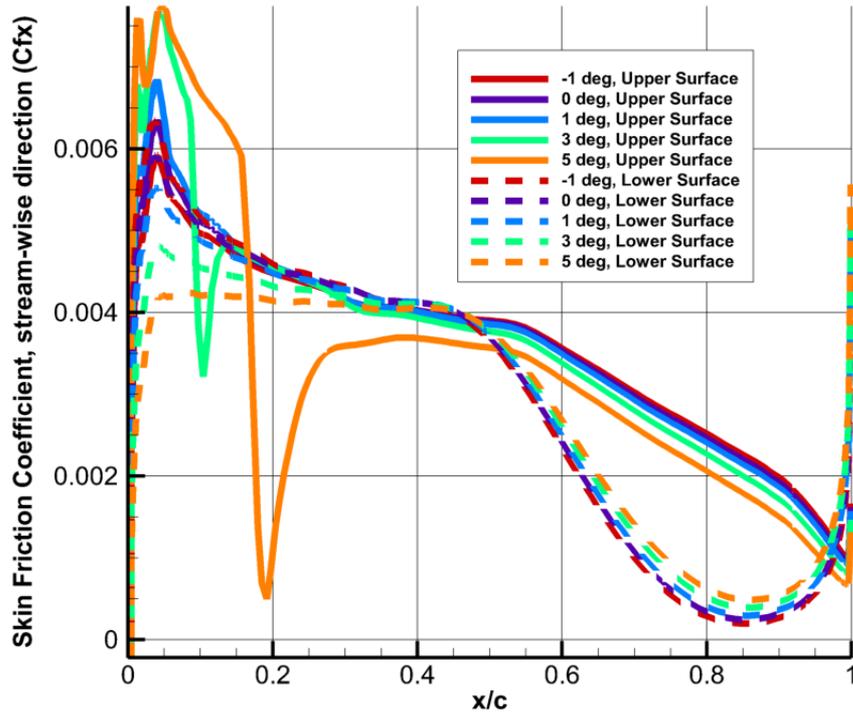


FUN3D Analysis, Medium Grid, Mach 0.82, Steady Rigid Analysis  
60% span station





FUN3D Analysis, Medium Grid, Mach 0.70, Steady Rigid Analysis  
60% span station



FUN3D Analysis, Medium Grid, Mach 0.70, Steady Rigid Analysis  
60% span station

